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Claims 1-10. (canceled)

Claim 11. (withdrawn) A method to derive selected physical properties of a sample passing successively through a set of detectors using a combination of the signals produced by said detectors responding to said sample passing therethrough when some of said detectors exhibit band broadening of their signals, comprising the steps of

- a) Applying a parameterized broadening function to said detector set to derive thereby a corresponding set of detector signals, all of which have comparable broadening; and
- b) Using said detector signals now broadened, following application of said broadening function, to derive said selected physical properties of said measured sample.

Claim 12. (withdrawn) The method of Claim 11 where said application of said parameterized broadening function is given by $D_i^b(t) = \int_{-\infty}^{\infty} D_i(t-\tau) B(\alpha_{ij}', \tau-\tau_i') d\tau$ where $D_i^b(t)$ are the said detector signals now broadened, α_{ij}' and τ_i' are said best fit parameters of Claim 2.

Claim 13. (withdrawn) The method of Claim 11 where said selected physical properties, to be determined from the relation $R(\theta) = K^* M_w c P(\theta) [1 - 2A_2 M_w c P(\theta)] + O(c^3)$, are the weight averaged molar mass, M_w , and the root mean square radius, r_g , of said sample derived from concentration signals, c(t), and the excess Rayleigh ratios, $R(\theta,t)$, derived from i light scattering signals from a detector set comprised of light scattering

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detectors, $D_i(t)$, and a dRI detector in sequence, said dRI detector producing a concentration signal exhibiting broadening relative to said light scattering detector signals, where said light scattering detector signals have been broadened.

Claim 14. (withdrawn) The method of Claim 11 where said detector signals are from a UV detector followed by a multiangle light scattering detector and said multiangle light scattering signals are broadened.

Claim 15. (withdrawn) The method of Claim 11 where said detector signals are from a refractive index detector followed by a viscometer detector and said refractive index detector signals are broadened.

Claim 16. (withdrawn) The method of 11 where said broadening function is given by

$$B(t) = \int_{-\infty}^{\infty} \frac{1}{\sigma \sqrt{2\pi}} e^{-\tau^2/2\sigma^2} \frac{1}{w} U(t-\tau) e^{-(t-\tau)/w} d\tau$$
, where U(t-\tau) = 1 when

 $t \ge \tau$ and =0 when $t < \tau$.

Claim 17. (withdrawn) The method of Claim16 where said optimal parameters of said broadening function have been determined by the method of Claim1.

Claim 18. (canceled)

Claim 19. (amended) A method to determine the best fit parameters of a broadening model to be used to correct for the effects of interdetector band broadening in a chromatographic separation containing a separation device followed by two or more

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detectors i = (1,n), where n is the number of detectors, comprising the steps of

- A. Selecting a broadening model $\underline{B(\alpha_0, \alpha_1, ..., \alpha_l, t)}$ containing a set of adjustable parameters $\underline{\alpha_j}$ (=0, ..., l), where l is the number of adjustable parameters;
- B. Injecting a reference sample;
- C. Collecting the <u>i</u> detector signals in time $D_i(t)$ as a function of time corresponding to a peak of uniform composition from each of said detectors of said sample, where a peak is defined as a range of time during which the sample of uniform composition elutes;
- D. defining Defining the most broadened peak as that corresponding to the peak having reference signal $D_n(t)$ as that which exhibits the broadest temporal response[[.]];
- E. For each detector *i*, Forming forming a $[\chi^2]$ model to be minimized over a peak of said sample to be broadened using said collected signal of the most broadened peak as a reference against which said other detector peaks are to be compared; which is derived from said broadening model, and is to be minimized over said peak using said signal $D_n(t)$ as a reference against which the said detector *i* is to be compared;

$$\chi_{i}^{2}\left(\beta_{i},\tau_{i},\alpha_{ij}\right) = \int_{peak} \left(D_{n}\left(t\right) - \beta_{i} \int_{-\infty}^{\infty} D_{i}\left(t - \tau\right) B\left(\alpha_{ij},\tau - \tau_{i}\right) d\tau\right)^{2} dt, \text{ where } \underline{\text{said best}}$$

$$\underline{\text{fit parameters are } \beta_{i},\alpha_{ij},\underline{\text{and } \tau_{i}};\underline{\text{ and}}}$$

(1) said best fit parameters are the β_i, α_{ij} , and τ_i ; and

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- (a) [[the]] β_i [[are]] is the scale factor[[s]] for detector i;
- (b) [[the]] α_{ij} characterizes the extent of the broadening for detector i and parameter j; and
- (c) [[the]] τ_i [[are]] is the interdetector time delay[[s]] for detector i.
- (2) the i detectors' responses as a function of time are the $D_i(t)$ and said model is minimized over said peak.
- F. Minimizing said $[\chi^2]$ models to determine yield said best fit parameters for each of said detector peaks to be broadened so that their broadened and normalized shapes are a best fit to said shape of said detector producing said broadest temporal response.

Claim 20. (amended) The method of Claim 19 where the minimization of said χ_i^2 models [[is]] are achieved by use of a nonlinear least squares algorithm.

Claim 21. (previously presented) The method of Claim 20 where said nonlinear least squares algorithm is of the type developed by Marquardt.

Claim 22. (amended) The method of Claim 19 where said <u>interdetector</u> band broadening is caused by dilution.

Claim 23. (amended) The method of Claim 19 where said <u>interdetector</u> band broadening is caused by mixing.

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Claim 24. (amended) The method of Claim 19 where said <u>interdetector</u> band broadening is caused by mechanical defects within the detector cells and/or connectors thereto.

Claim 25. (amended) The method of Claim 19 where said <u>interdetector</u> band broadening is caused by internal instrumental averaging.

Claim 26. (previously presented) The method of Claim 25 where said internal instrumental averaging is from electronic filtering.

Claim 27. (previously presented) The method of Claim 25 where said internal instrumental averaging is by measuring a range of volumes of the sample.

Claim 28. (previously presented) The method of Claim 19 where said peaks of uniform composition correspond to monodisperse fractions which are separated from the other fractions by said chromatographic separation.

Claim 29. (amended) The method of Claim 19 where said peaks of uniform composition correspond respectively to fractions for which said ehromatographic separation device is ineffective and produces no appreciable separation so that said sample elutes with a uniform composition.

Claim 30. (amended) The method of Claim 19 where said broadening model is given by

$$B(\alpha_1, \alpha_2, t) = \int_{-\infty}^{\infty} \frac{1}{\alpha_1 \sqrt{2\pi}} e^{-\tau^2/2\alpha_1^2} \frac{1}{\alpha_2} U(t - \tau) e^{-(t - \tau)/\alpha_2} d\tau, \text{ where } \alpha_1 \text{ and } \alpha_2 \text{ are parameters}$$

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that characterize said interdetector band broadening; the parameter α_1 characterizes Gaussian broadening due to internal instrumental averaging, and α_2 characterizes an interdetector mixing volume; and where $U(t-\tau)=1$ when $t \ge \tau$ and $U(t-\tau)=0$ and when $t < \tau$.